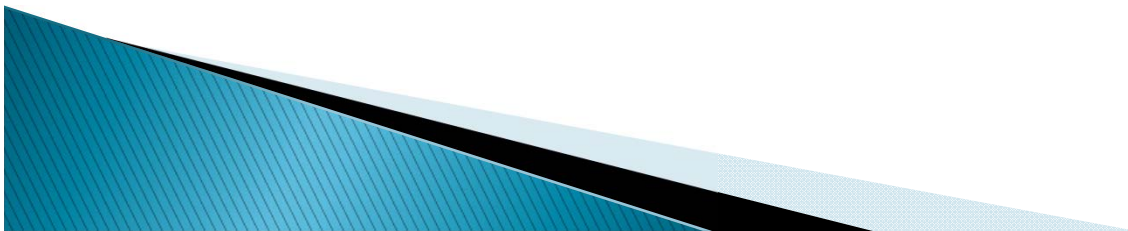


Separation of Mock Used Fuel and Mock Glass Debris using Eichrom Resins

Radiobioassy and Radiochemical Measurement Conference
Audrey Roman, Rebecca Springs, Evelyn Bond, Ralf Sudowe
October 28, 2014

LA-UR -14-28270

Mock Used Fuel



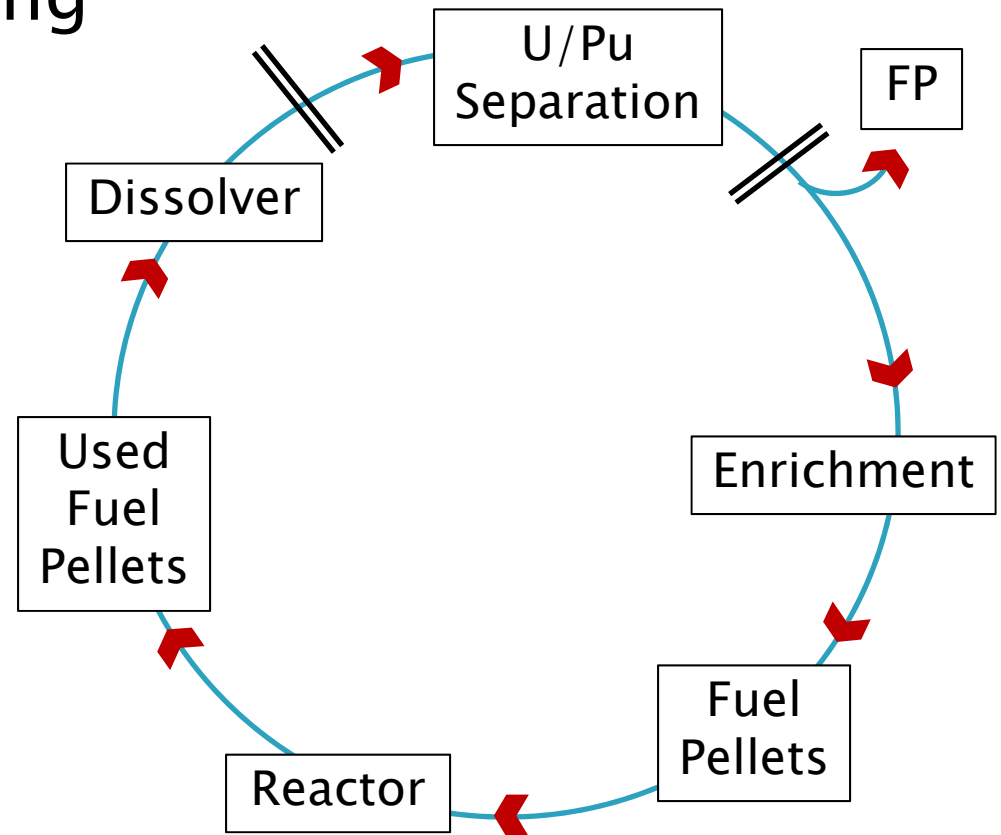
Safeguards

- ▶ Material Accountancy (IAEA)
 - Special Nuclear Material: Pu-239, U-233, and U-235
 - Near Real Time Accountancy (NRTA)
 - Homogenous Samples
 - Batch Data
 - “Source data may include, for example, ... element concentration, isotopic ratios, relationship between volume and manometer readings and relationship between plutonium produced and power generated”

Material Accountancy of Used Fuel

▶ Spent Fuel Reprocessing Streams

- Spent Fuel Composition
- PUREX process
- Possible contaminants



Safeguard Analytical Methods for the Nuclear Fuel Cycle

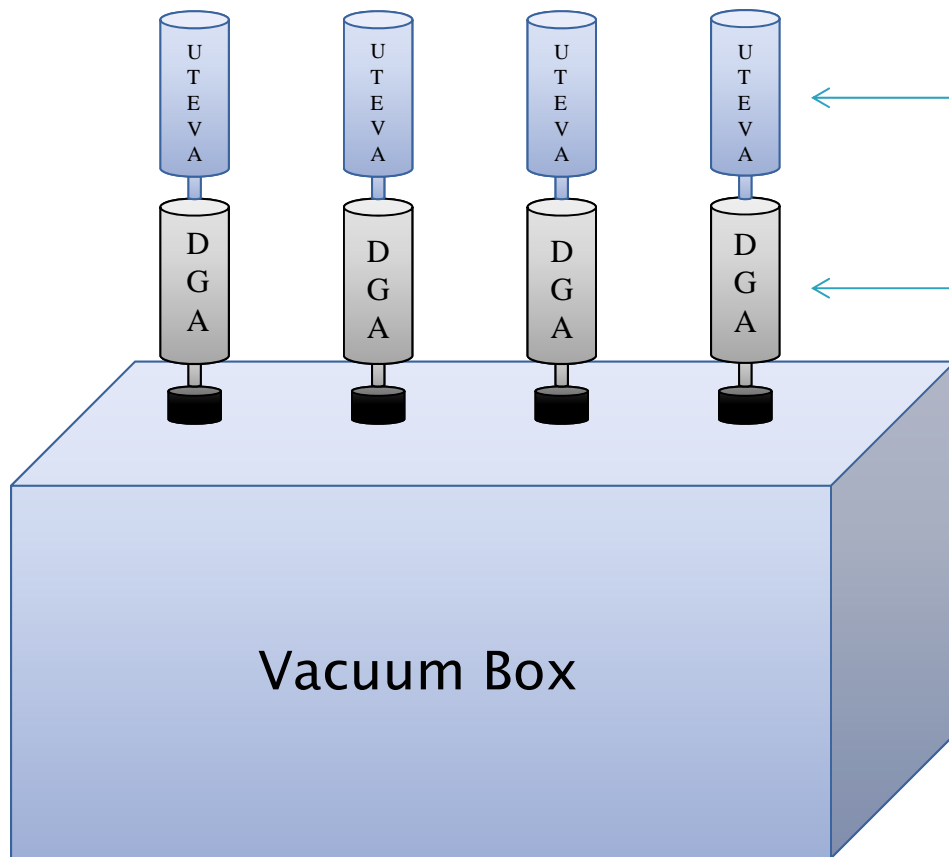
Current Method

- ▶ Hybrid K-Edge (HKED)
 - XRF and KED
 - Very accurate
 - Only detects concentration

Proposed Method

- ▶ Inductively Coupled Plasma – Mass Spectrometer (ICP-MS)
 - Very accurate
 - Detects concentration of isotopes
 - Numerous isobaric overlaps for actinides
 - Need chemistry of samples prior to analysis

Automated Elution Scheme



Scheme 1

Adsorbent (VI)
U(IV)

Adsorbent (IV)
Am(III)
Pu(III)

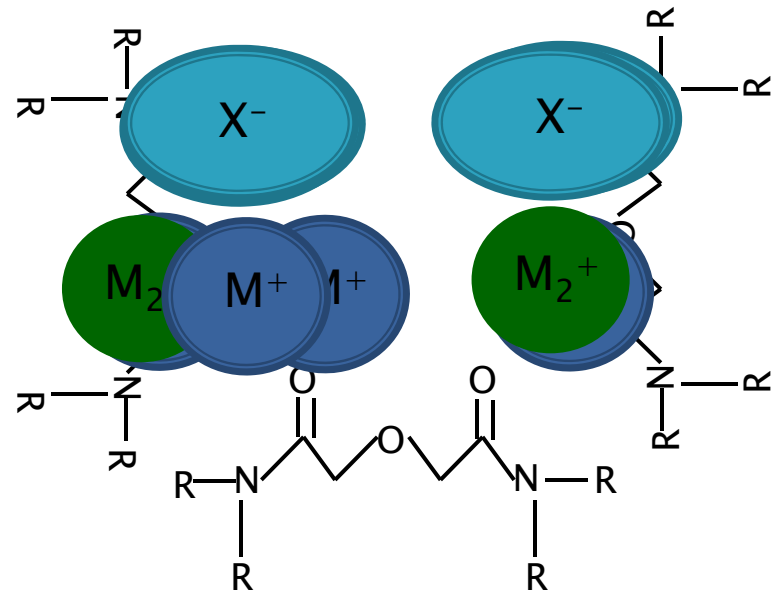
Scheme 2

Adsorbent (III)
Am(III) and
Pu(III)

Adsorbent (III)
Americium

Component Effects on Adsorption

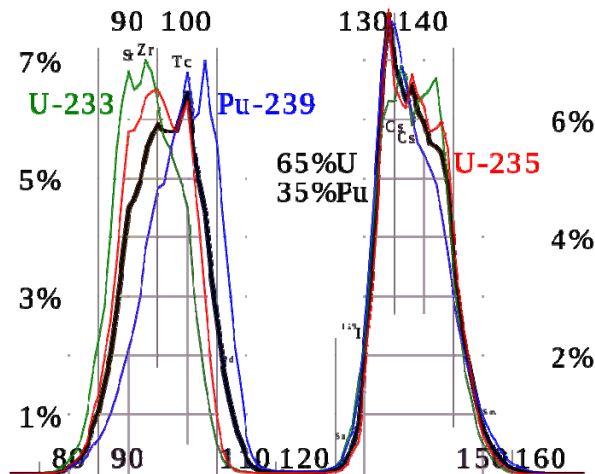
- ▶ Synergistic Effect
 - The combined species has a higher affinity than the individual species
- ▶ Antagonistic Effect
 - The combined species has a lower affinity than the individual species
- ▶ Competition Effect
 - The additional component competes with another metal for adsorption sites, lowering the number of available sites



Used Fuel Components

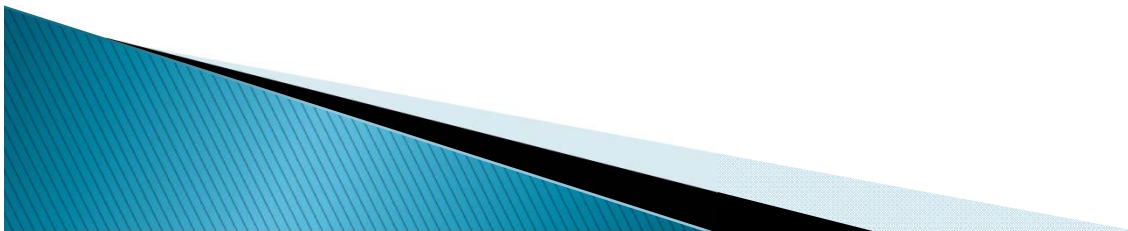
ORIGIN calculation for mass percentages are based on:

1. 30 MWd/kg M burnup
2. 10 year cool down period
3. 2.9% initial ^{235}U enrichment

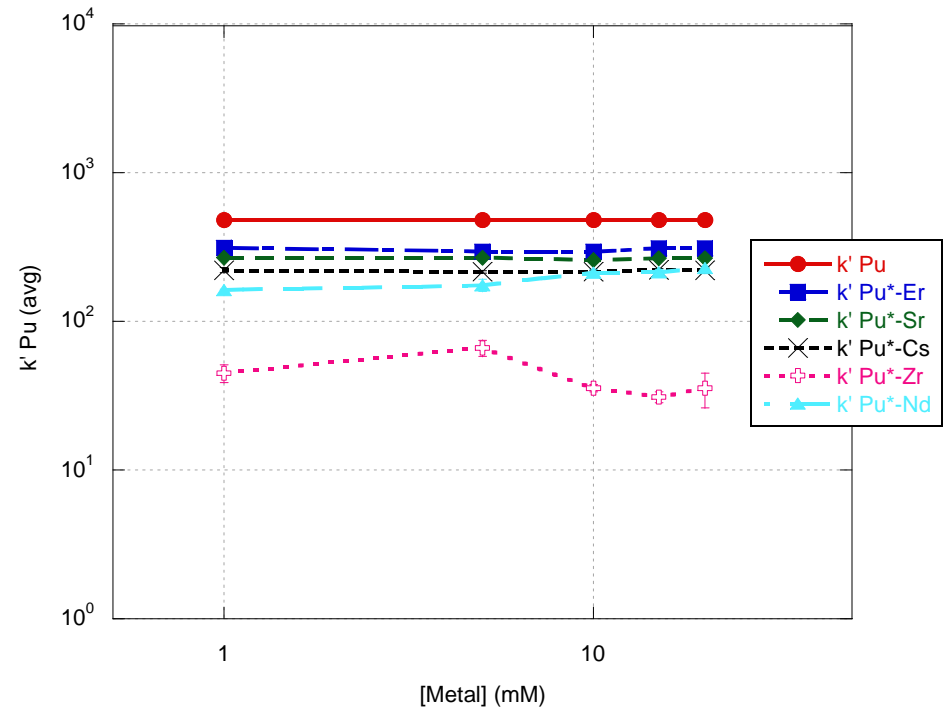
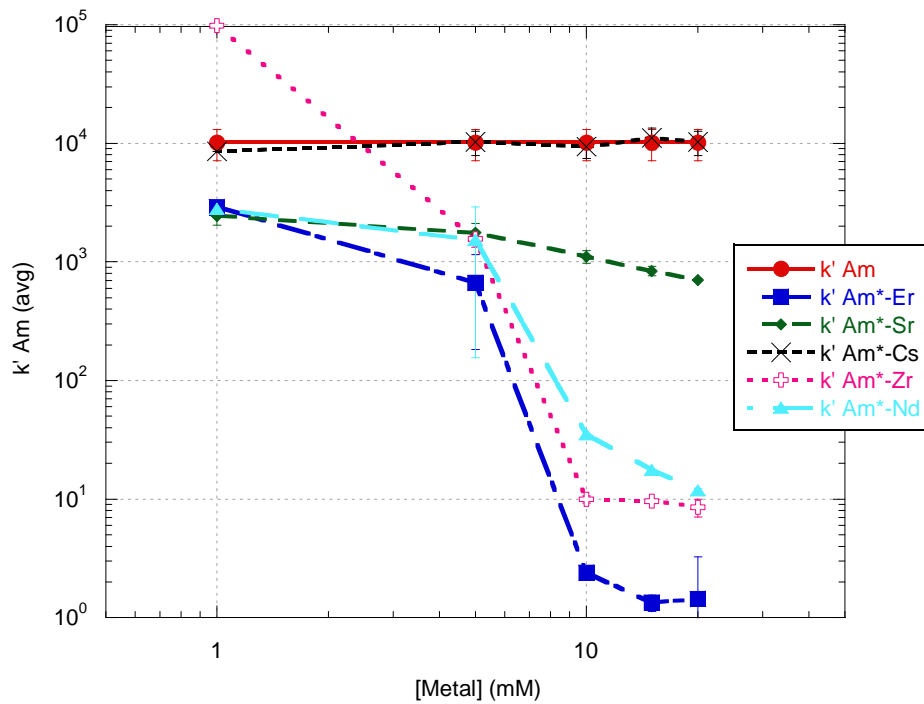


| Ranked by Mass | | |
|----------------|---------|---------|
| Rank | Element | Percent |
| 1 | U | 98.43 |
| 2 | Pu | 0.85 |
| 3 | Nd | 0.13 |
| 4 | Cs | 0.13 |
| 5 | Ce | 0.1 |
| 6 | Tc | 0.07 |
| 7 | Zr | 0.07 |
| 8 | Am | 0.06 |
| 9 | Np | 0.04 |
| 10 | Sr | 0.04 |
| 11 | Rb | 0.02 |
| 12 | Sm | 0.02 |
| 13 | I | 0.02 |
| 14 | Cm | 0.01 |
| 15 | Sn | <0.00 |

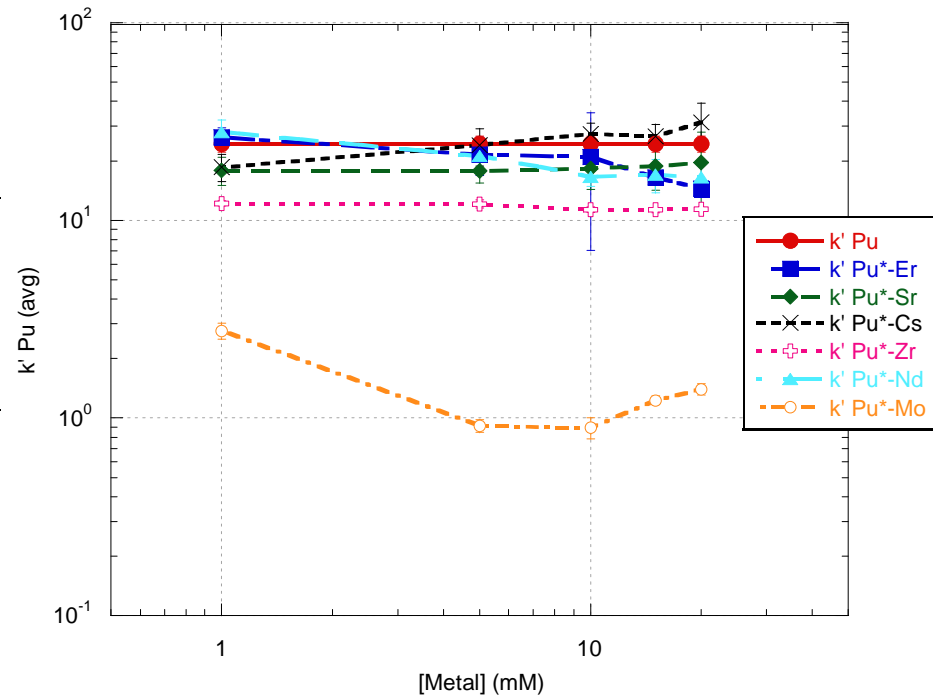
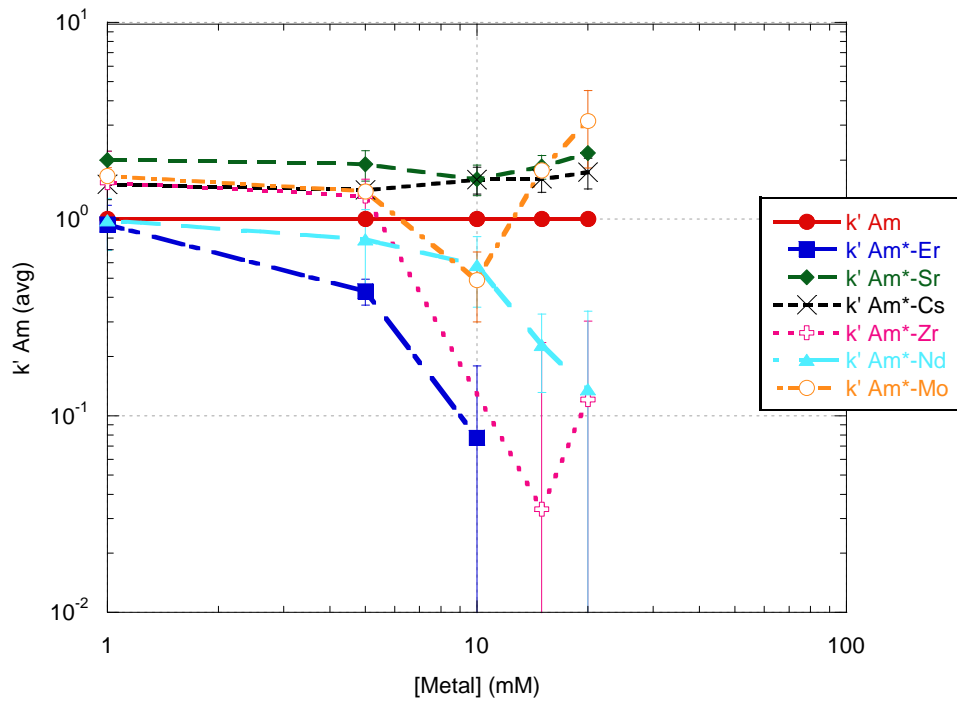
Characterization of Am and Pu Adsorption to DGA Resin in 1 M HNO₃ and HCl



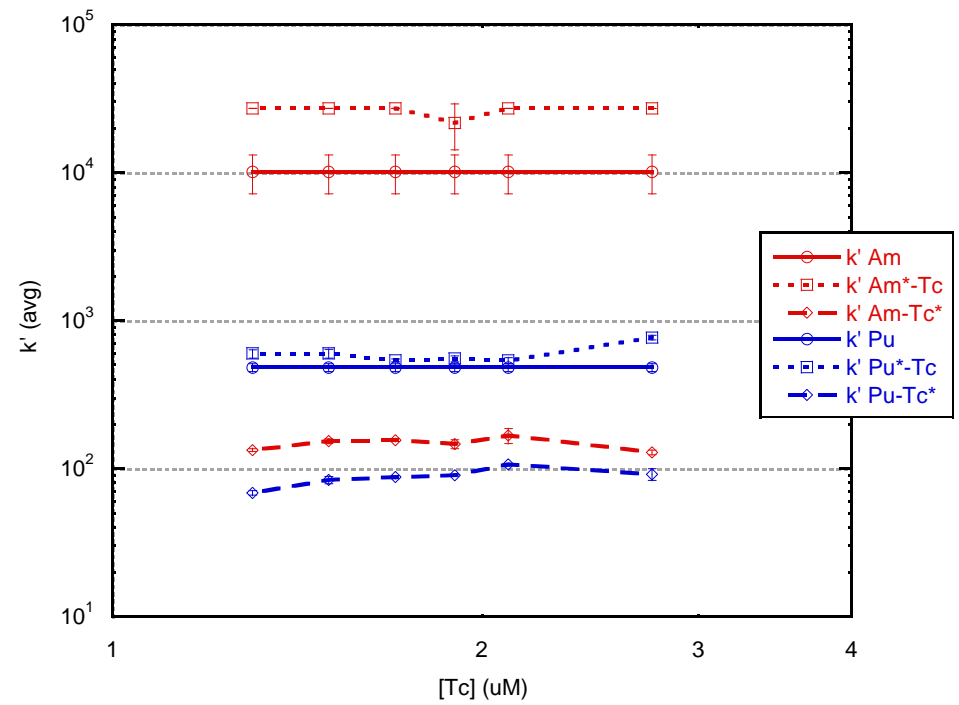
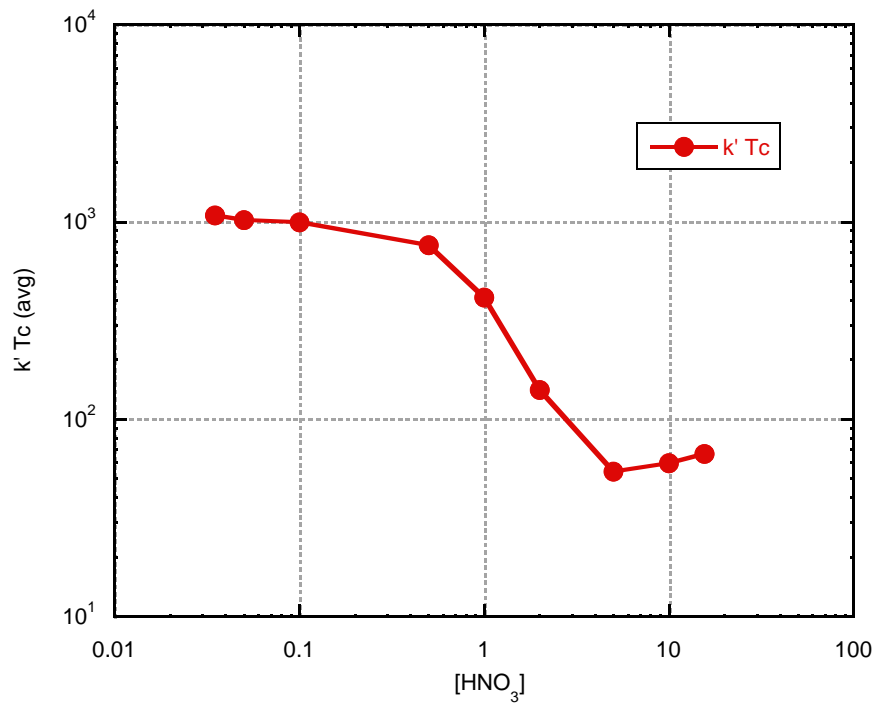
Component Effects on Am and Pu Adsorption to DGA Resin in 1 M HNO₃



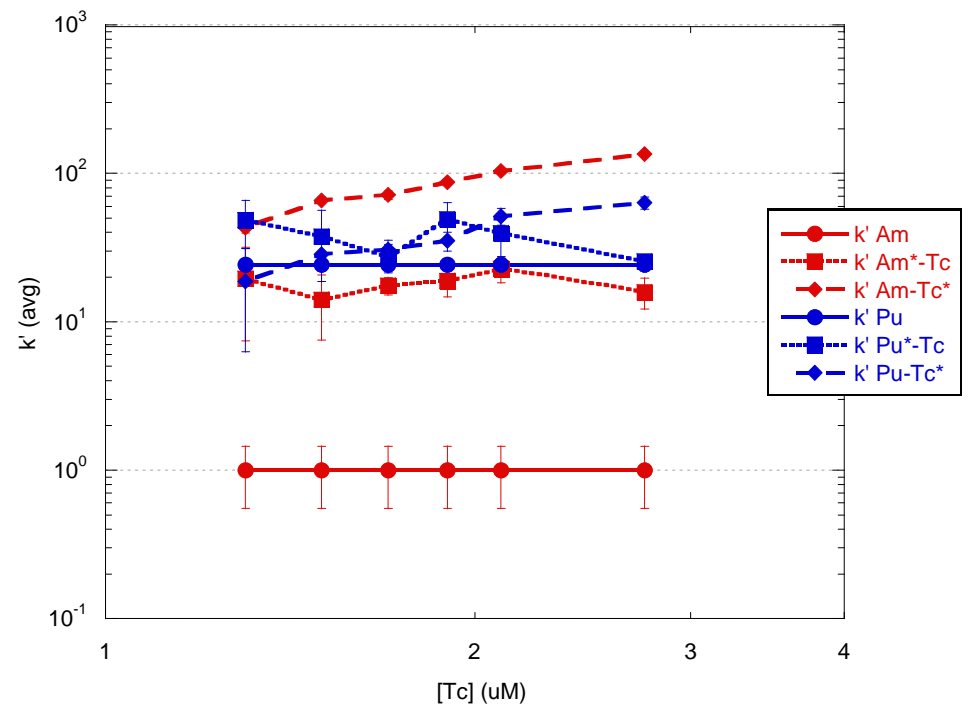
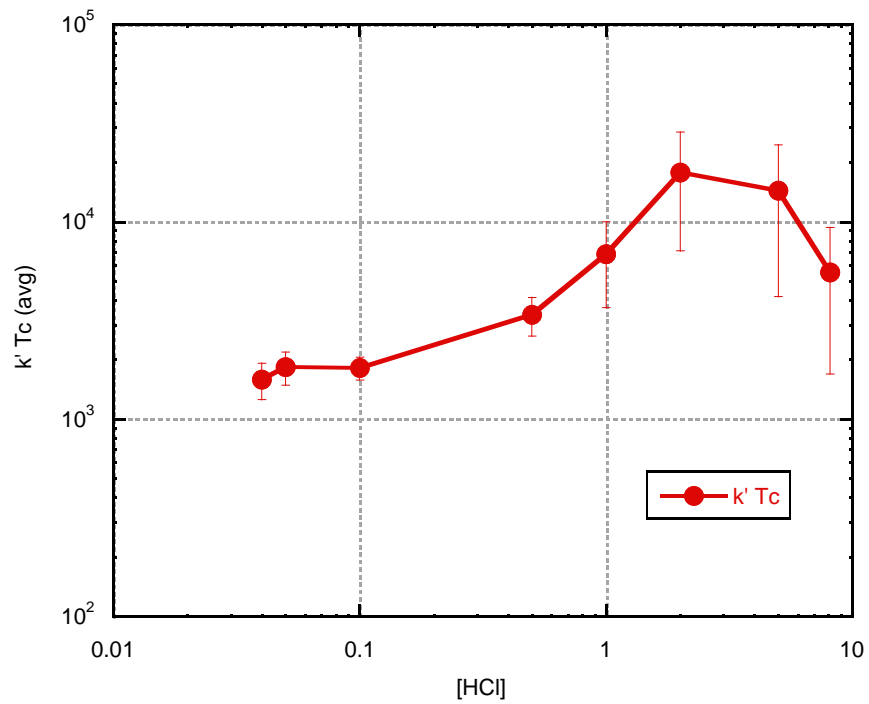
Component Effects on Am and Pu Adsorption to DGA Resin in 1 M HCl



Technetium Characteristics on DGA in 1 M HNO₃



Technetium Characteristics on DGA in 1 M HCl



Conclusions on Am, Pu Adsorption to DGA Resin

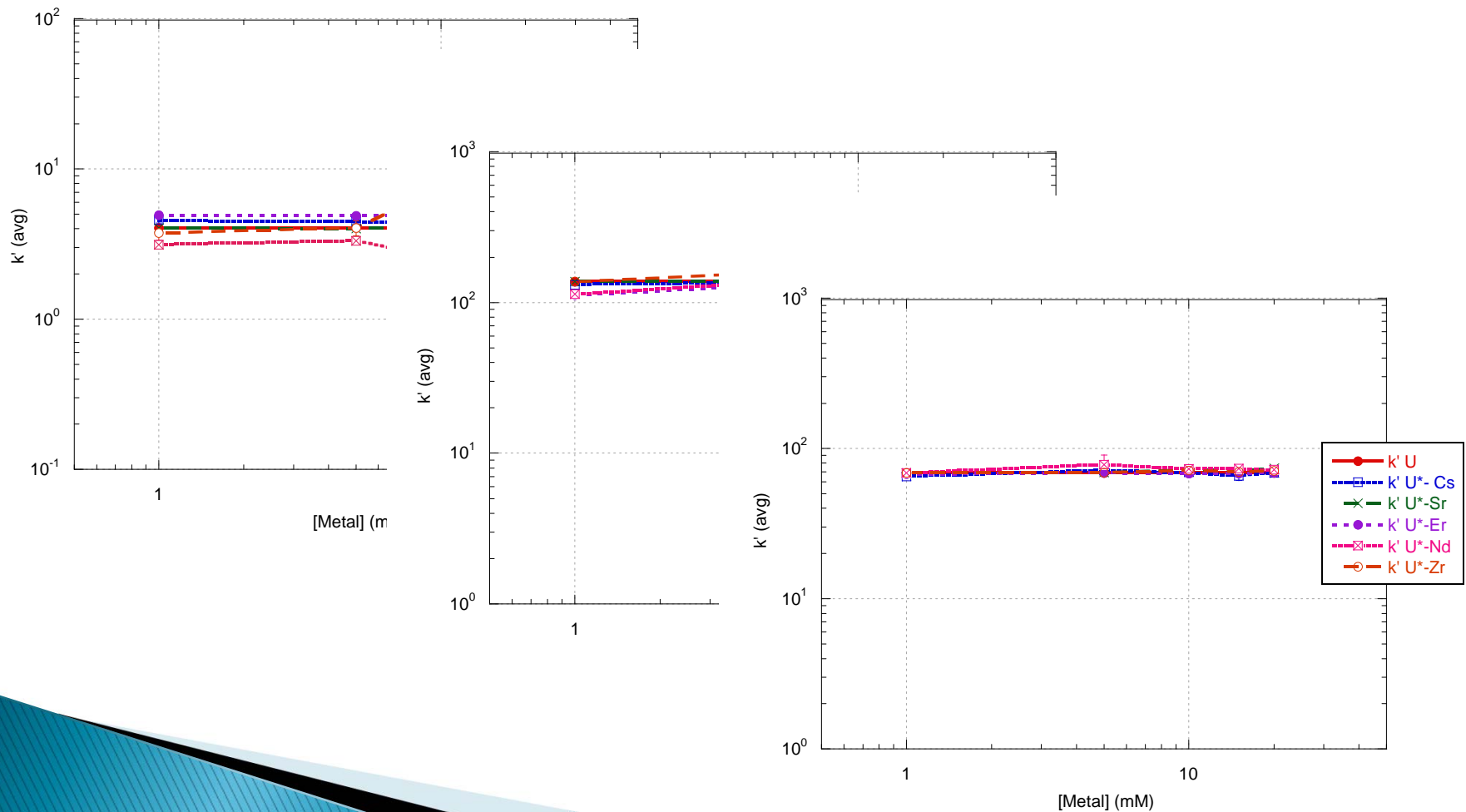
- ▶ 5M HNO₃ loading phase seems highly viable since Am and Pu adsorption in 1M HNO₃ is not considerably affected
 - Lanthanides and trivalent actinides are expected to be found in similar elution fractions
- ▶ Working capacity of the resin must be determined for DGA based on all trivalent metals
- ▶ TcO₄⁻ shows a synergistic effect on Am adsorption in 1M HCl acid



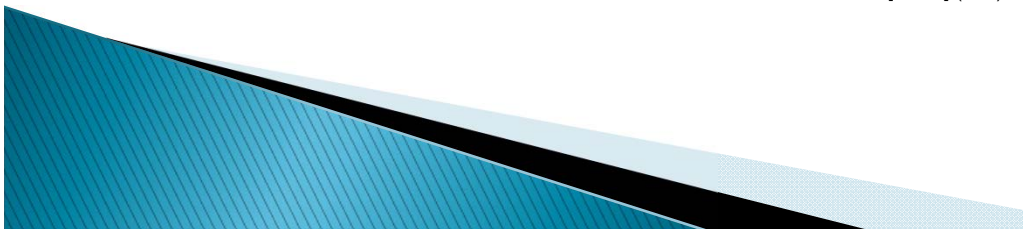
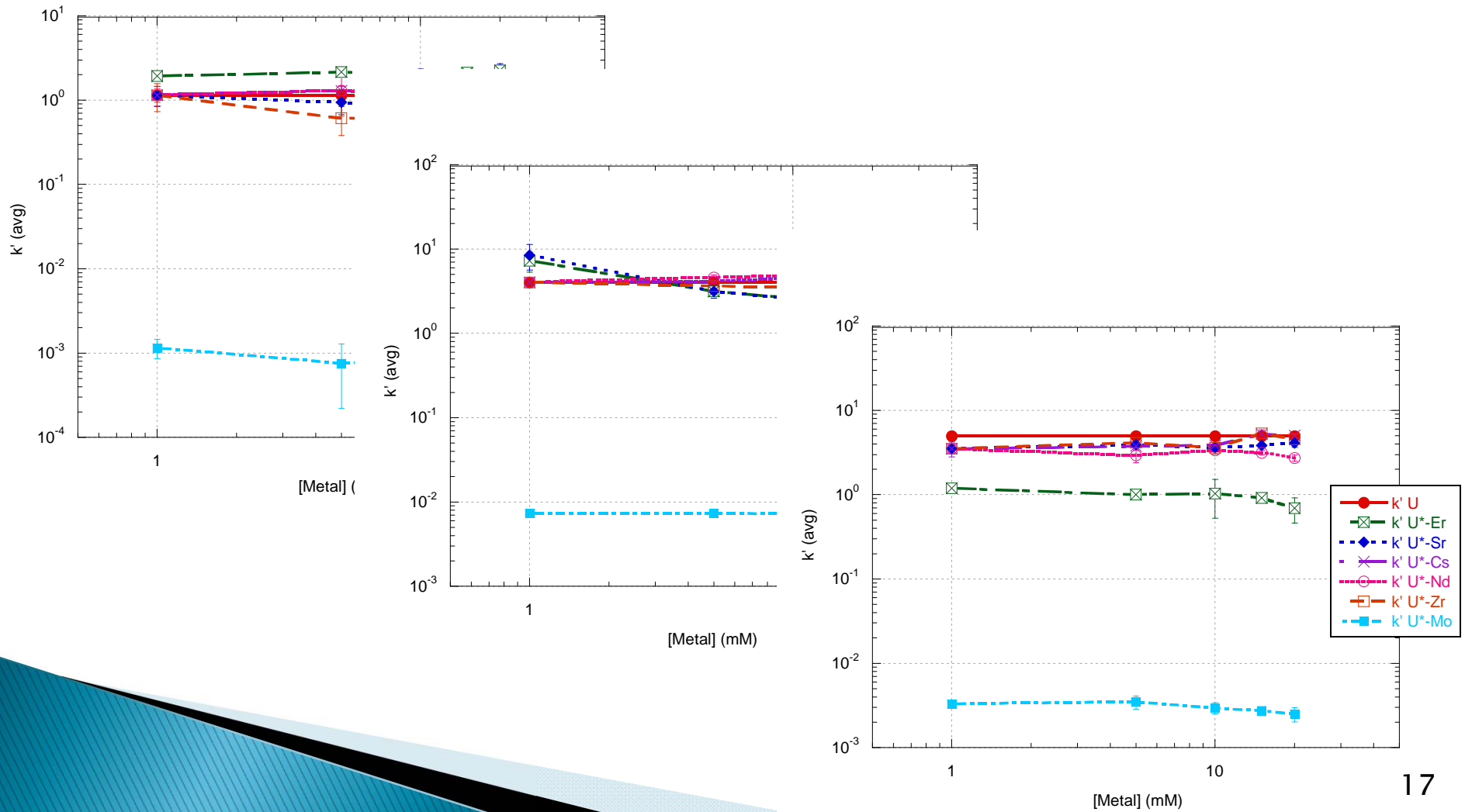
Characterization of Am, Pu and U Adsorption to UTEVA Resin in 1 M HNO₃ and HCl



Component Effects on Am, Pu and U Adsorption to UTEVA Resin in 1 M HNO₃



Component Effects on Am, Pu and U Adsorption to UTEVA Resin in 1M HCl

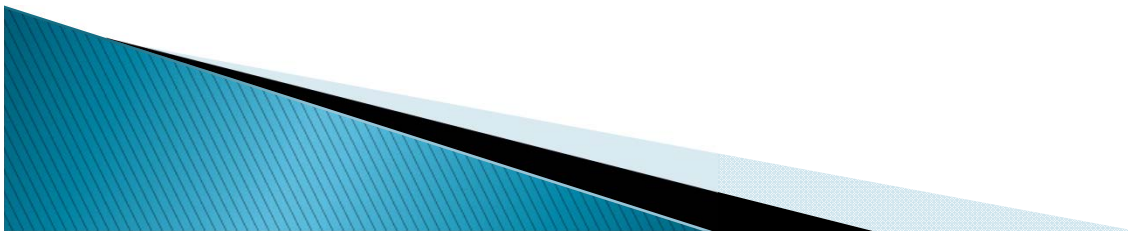


Conclusions on Am, Pu, and U Adsorption to UTEVA Resin

- ▶ No effects seen from additional components in 1M HNO₃
 - Loading characteristics should remain unchanged for used fuel
- ▶ Molybdenum antagonistic effects most likely due to the formation of complex oxyanions
- ▶ Overall, UTEVA very selective to tetra- and hexavalent metals



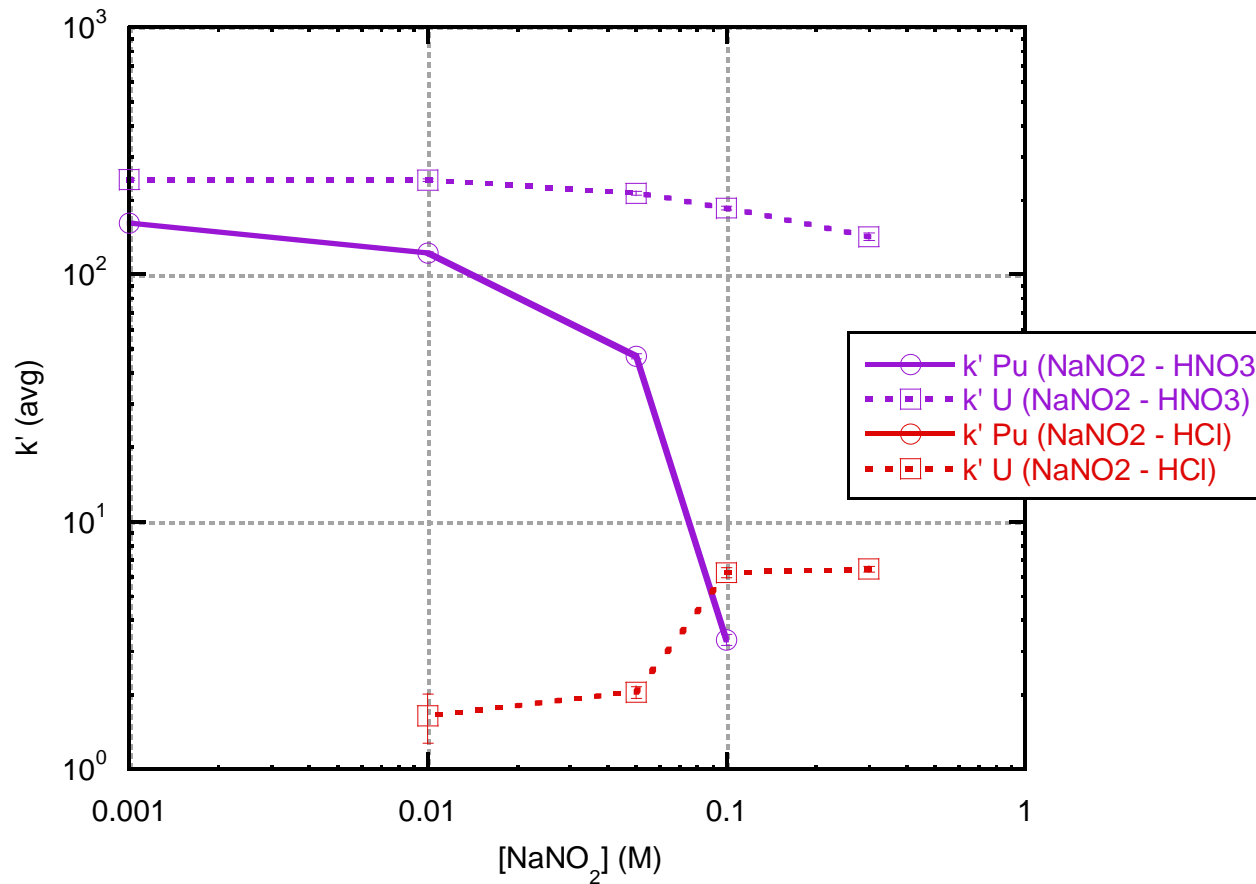
Investigation of Varying Matrices



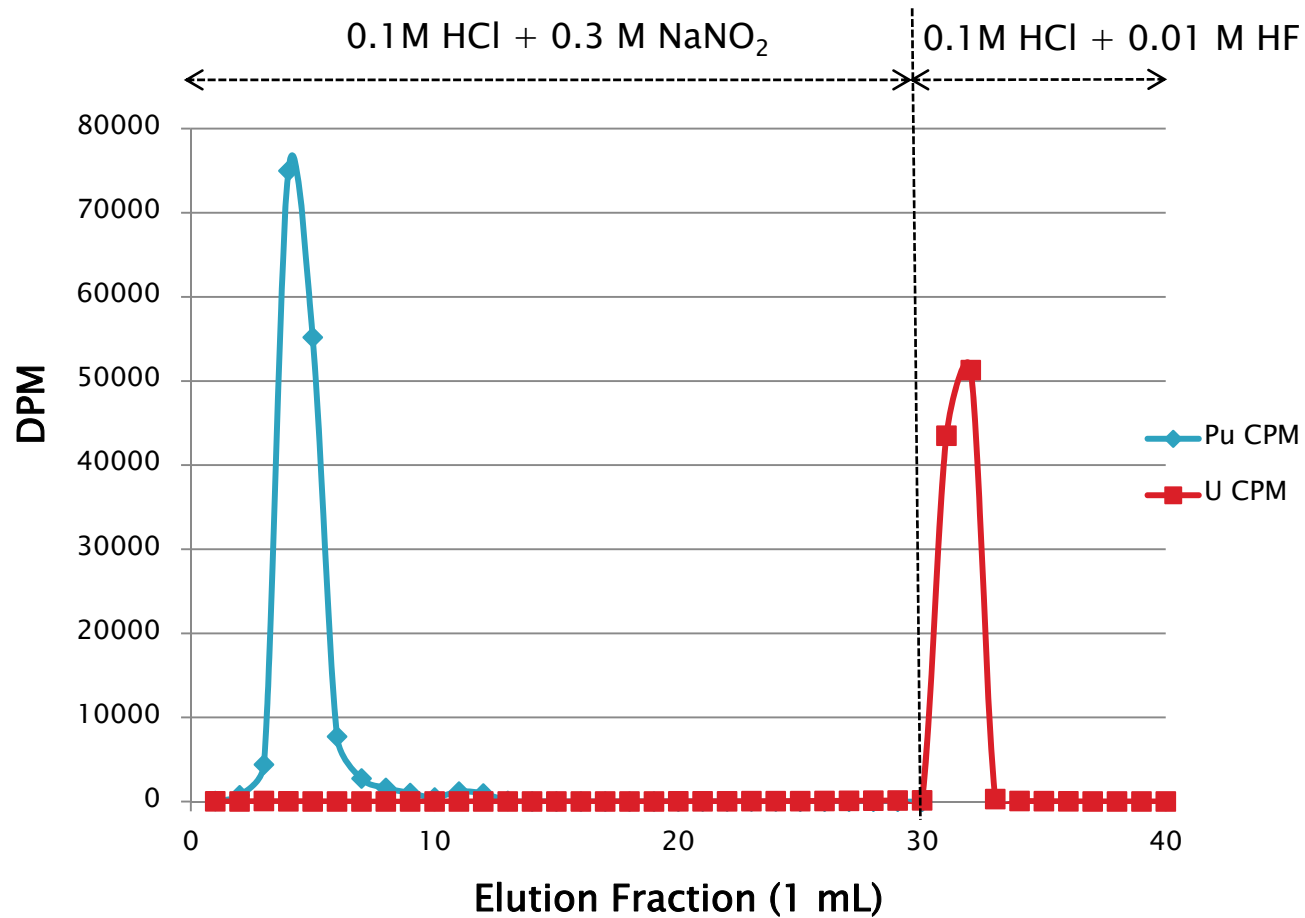
Summary of Varying Matrices Studied

| Matrix Constituents | Concentrations (M) | DGA | UTEVA |
|---|---|------------|---------------|
| HNO ₃ | 0.035, 0.05, 0.5, 1.0, 5.0, 10.0, 10.57 | Am, Cm, Pu | Am, Cm, Pu, U |
| HCl | 0.035, 0.05, 0.1, 0.5, 2.0, 5.0, 8.1 | Am, Cm, Pu | Am, Cm, Pu, U |
| H ₂ SO ₄ | 0.25, 0.5, 0.7, 1, 2, 3, 4 | Am, Cm, Pu | |
| HI | 0.001, 0.007, 0.015, 0.1, 0.145 | Am, Cm, Pu | |
| HBr | 0.001, 0.007, 0.015, 0.1, 0.145 | Am, Cm, Pu | |
| NaSO ₄ + 1M HNO ₃ | 0.1, 0.5, 1.0, 1.5, 2.0 | Am, Cm, Pu | |
| NaSO ₄ + 1M HCl | 0.1, 0.5, 1.0, 1.5, 2.0 | Am, Cm, Pu | |
| NaBr + 1M HNO ₃ | 0.01, 0.1, 0.5, 1.0, 4.0 | Am, Cm, Pu | |
| NaBr + 1M HCl | 0.01, 0.1, 0.5, 1.0, 4.0 | Am, Cm, Pu | |
| NaNO ₂ + 1M HNO ₃ | 0.001, 0.01, 0.05, 0.1, 0.5 | Am, Cm, Pu | Am, Pu, U |
| NaNO ₂ + 1M HCl | 0.001, 0.01, 0.05, 0.1, 0.6 | Am, Cm, Pu | Am, Pu, U |
| Ascorbic Acid + 1M HNO ₃ | 0.001, 0.01, 0.05, 0.1, 0.3 | Am, Cm, Pu | Am, Pu, U |
| Ascorbic Acid + 1M HCl | 0.001, 0.01, 0.05, 0.1, 0.3 | Am, Cm, Pu | Am, Pu, U |
| Oxalic Acid + 1M HNO ₃ | 0.001, 0.01, 0.05, 0.1, 0.3 | Am, Cm, Pu | Am, Pu, U |
| Oxalic Acid + 1M HCl | 0.001, 0.01, 0.05, 0.1, 0.3 | Am, Cm, Pu | Am, Pu, U |

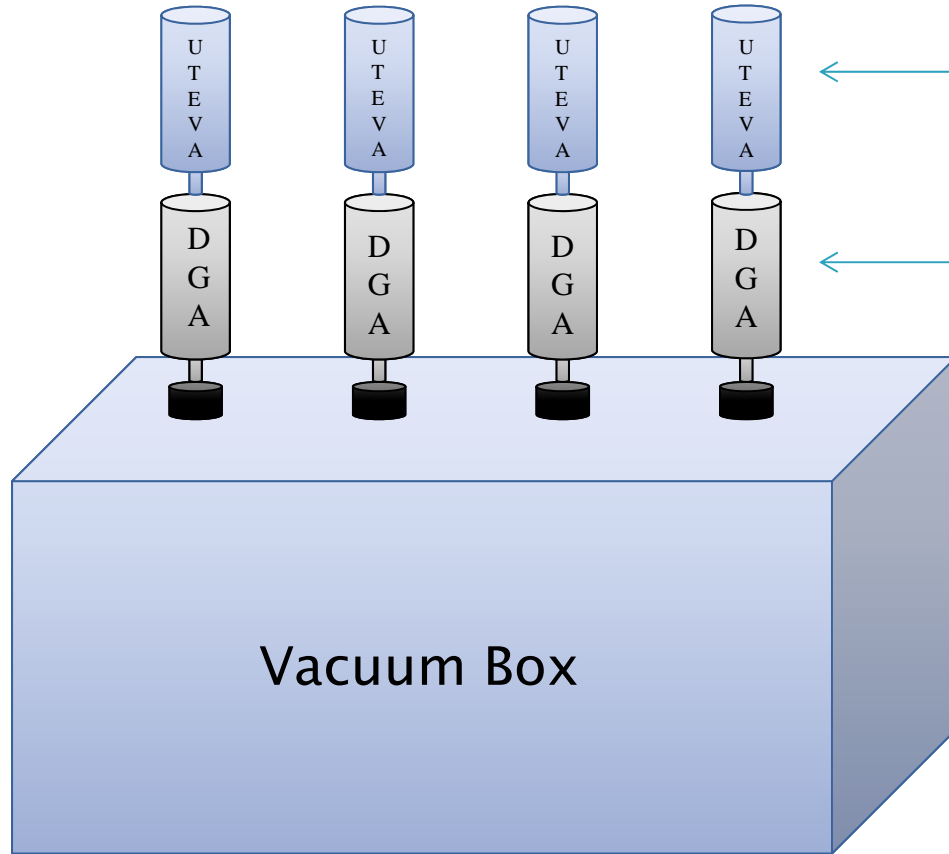
Pu, and U Adsorption to UTEVA in NaNO_2



Pu and U separation on UTEVA



Conclusions from Elution Profile Characterizations



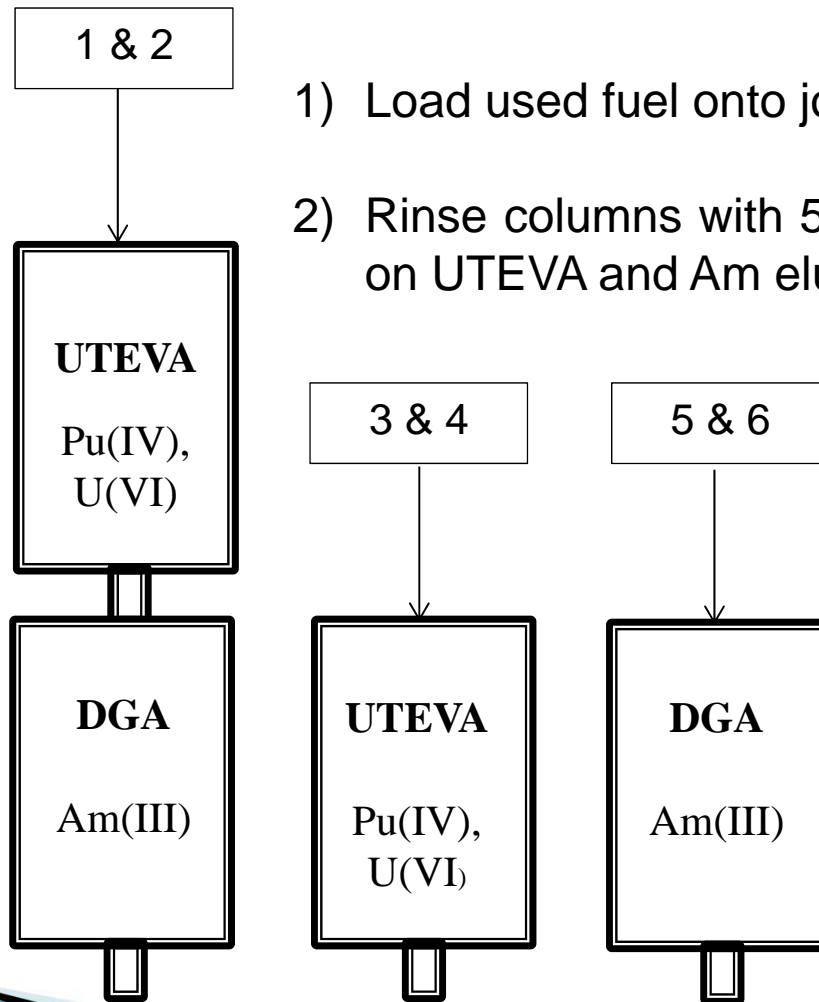
Scheme 2

~~Alderson~~ Pu(III)
~~Am(III) strip~~ and
~~Elution~~ Americium

~~Alderson~~ Am(III)
Americium



Proposed Used Fuel Separation



1) Load used fuel onto joined columns using 5M HNO₃.

2) Rinse columns with 5M HNO₃, Pu and U are retained on UTEVA and Am elutes through to DGA

3) Pu(III) Elution:
0.1 M HCl + 0.3M NaNO₂

4) U(IV) Elution:
0.1 M HCl + 0.01 M HF

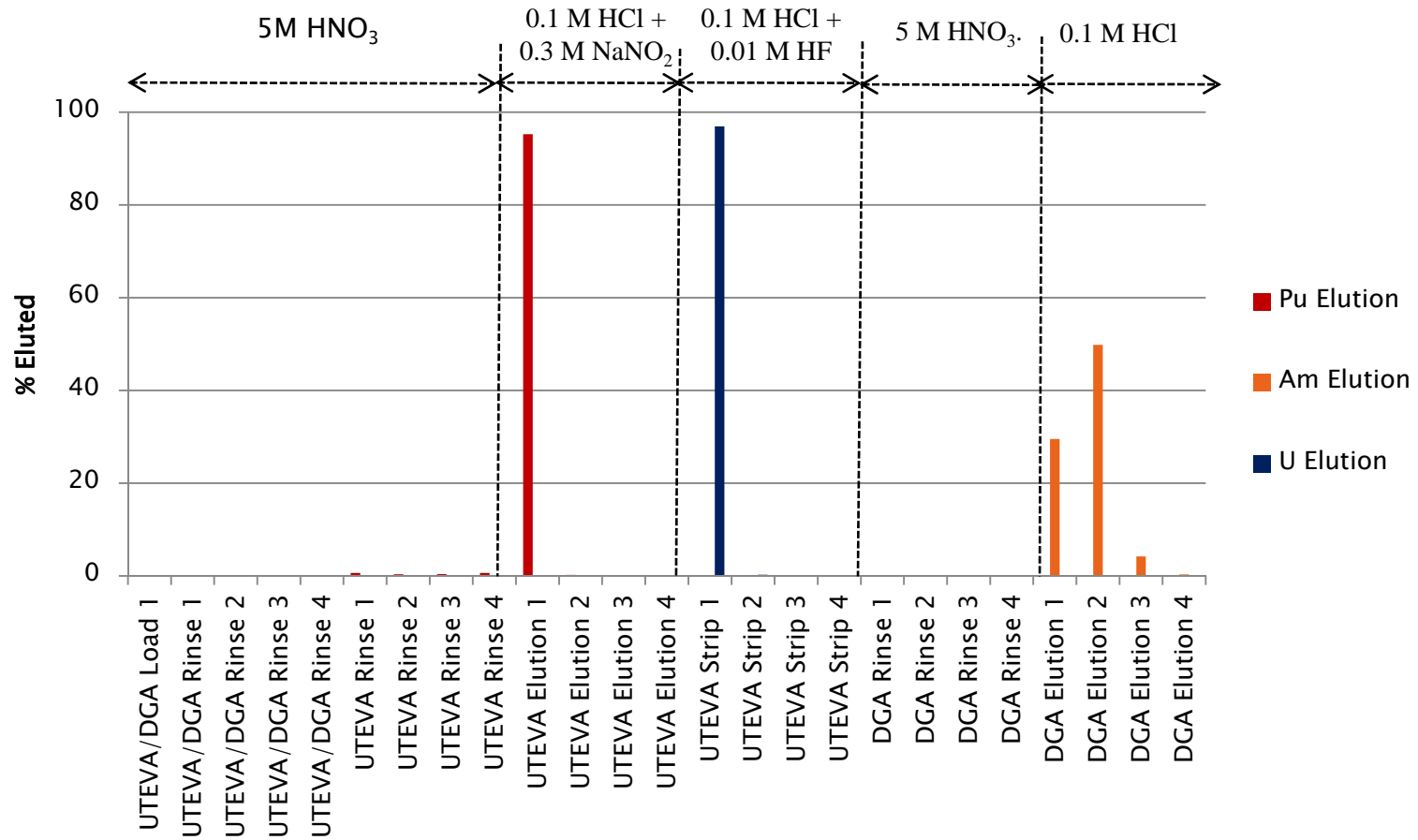
5) Am(III) Elution:
0.1 M HCl.

6) Strip:
0.1 M HCl + 0.01 M HF

Vacuum Box Separations



Actinide Separation on Vacuum Box



2mL prepacked cartridges,
5mL fractions

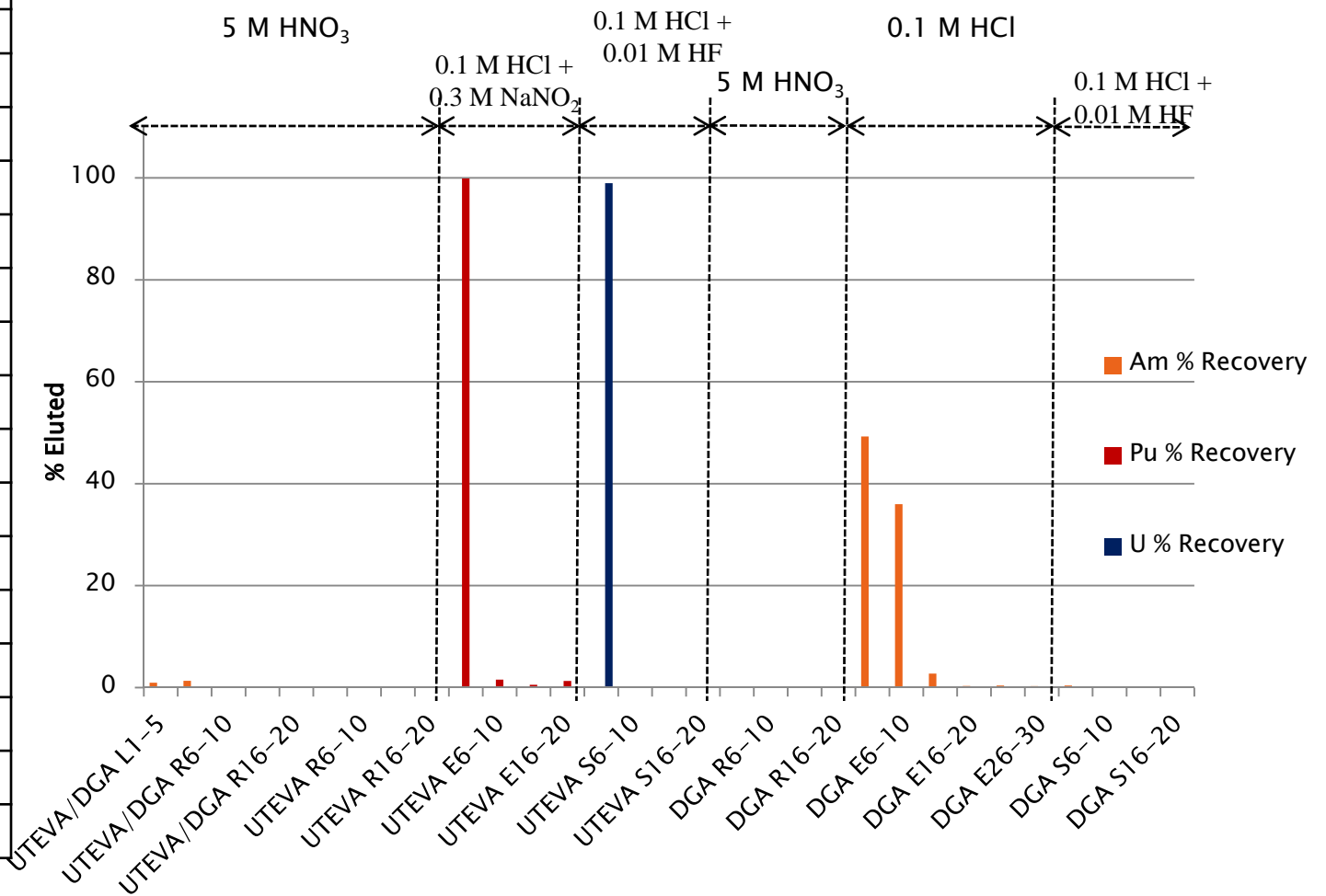
Actinide Separation Conclusion

- ▶ Pu and U had sharp elution peaks
- ▶ Am had broad elution from DGA resin
 - Most likely due to the elevated flow rates
- ▶ Further broadening expected for mock used fuel separation

| | % Recovery | STD |
|--------|------------|-------|
| Am-241 | 95.01 | 14.04 |
| Pu-239 | 95.54 | 0.06 |
| U-233 | 97.29 | 0.68 |

Rapid Mock Used Fuel Separation

| Ranked by Mass | | |
|----------------|---------|---------|
| Rank | Element | Percent |
| 1 | U | 98.43 |
| 2 | Pu | 0.85 |
| 3 | Nd | 0.13 |
| 4 | Cs | 0.13 |
| 5 | Ce | 0.1 |
| 6 | Tc | 0.07 |
| 7 | Zr | 0.07 |
| 8 | Am | 0.06 |
| 9 | Np | 0.04 |
| 10 | Sr | 0.04 |
| 11 | Rb | 0.02 |
| 12 | Sm | 0.02 |
| 13 | I | 0.02 |
| 14 | Cm | 0.01 |
| 15 | Sn | <0.00 |



Conclusions

- ▶ Overall, recoveries were still high but had large deviations
- ▶ Some additional broadening in Pu elution
- ▶ Am elution characteristics varied
 - Most likely due to the addition of Tc-99

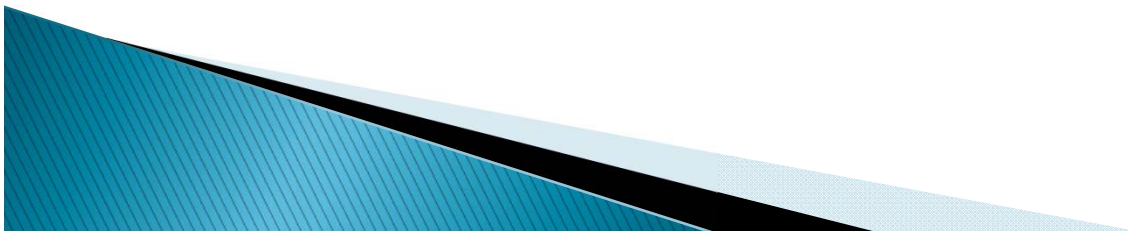
| | % Recovery | STD |
|--------|------------|-------|
| Am-241 | 92.68 | 39.60 |
| Pu-239 | 99.18 | 1.65 |
| U-233 | 103.29 | 5.27 |

Overall Conclusions

- ▶ UTEVA worked great
- ▶ Scheme 2 is viable and promising
- ▶ Replace DGA possibly with another extraction chromatography resin
 - TRU



Melt Glass Bead Separation



Mock Melt Glass

- ▶ Mixture of glass and cement to represent melt glass and urban debris
- ▶ Typically a 2 gram sample
- ▶ Long digestion process

| Material | Main Compounds |
|----------|--|
| Glass | SiO_2 , Na_2O , CaO , MgO , Al_2O_3 |
| Cement | CaO , SiO_2 , Al_2O_3 , Fe_2O_3 , $\text{CaSO}_4 \cdot \text{H}_2\text{O}$ |



Expected Activation Products

| Element | Isotope | Natural Abundance (%) [135] | Neutron Cross Section (barns) [136]* | (n,p) Product | Product T _{1/2} (unless noted otherwise) |
|----------|---------|-----------------------------|--------------------------------------|---------------------------------------|---|
| Titanium | 48 | 73.72 | 0.05927 | ⁴⁸ Sc | 43.67 h |
| | 46 | 8.25 | 0.2893 | ⁴⁶ Sc | 83.79 d |
| | 47 | 7.44 | 0.14503 | ⁴⁷ Sc | 3.349 d |
| | 49 | 5.41 | 0.0512 | ⁴⁹ Sc | 57.18 m |
| | 50 | 5.18 | 0.0113 | ⁵⁰ Sc | 102.50 m |
| Iron | 56 | 91.75 | 0.11436 | ⁵⁶ Mn | 2.58 h |
| | 54 | 5.8 | 0.33447 | ⁵⁴ Mn | 312.12 d |
| | 57 | 2.12 | 0.05705 | ⁵⁷ Mn | 85.40 s |
| Nickel | 58 | 68.07 | 0.36358 | ⁵⁸ Co | 70.86 d |
| | 60 | 26.22 | 0.1456 | ⁶⁰ Co | 1925.28 d |
| | 62 | 3.63 | 0.03117 | ⁶² Co | 1.50 m |
| | 61 | 1.14 | 0.09473 | ⁶¹ Co | 1.65 h |
| Gold** | 197 | 100 | 0.00188 | ¹⁹⁷ Pt | 19.89 h |
| | 196 | n/a | 0.0056 | ¹⁹⁶ Pt _(stable) | ¹⁹⁶ Au, 6.17 d |
| | 195 | n/a | 0.003083 | ¹⁹⁵ Pt _(stable) | ¹⁹⁵ Au, 186.09 d |

*14.1 MeV neutron energy, for n,p reactions

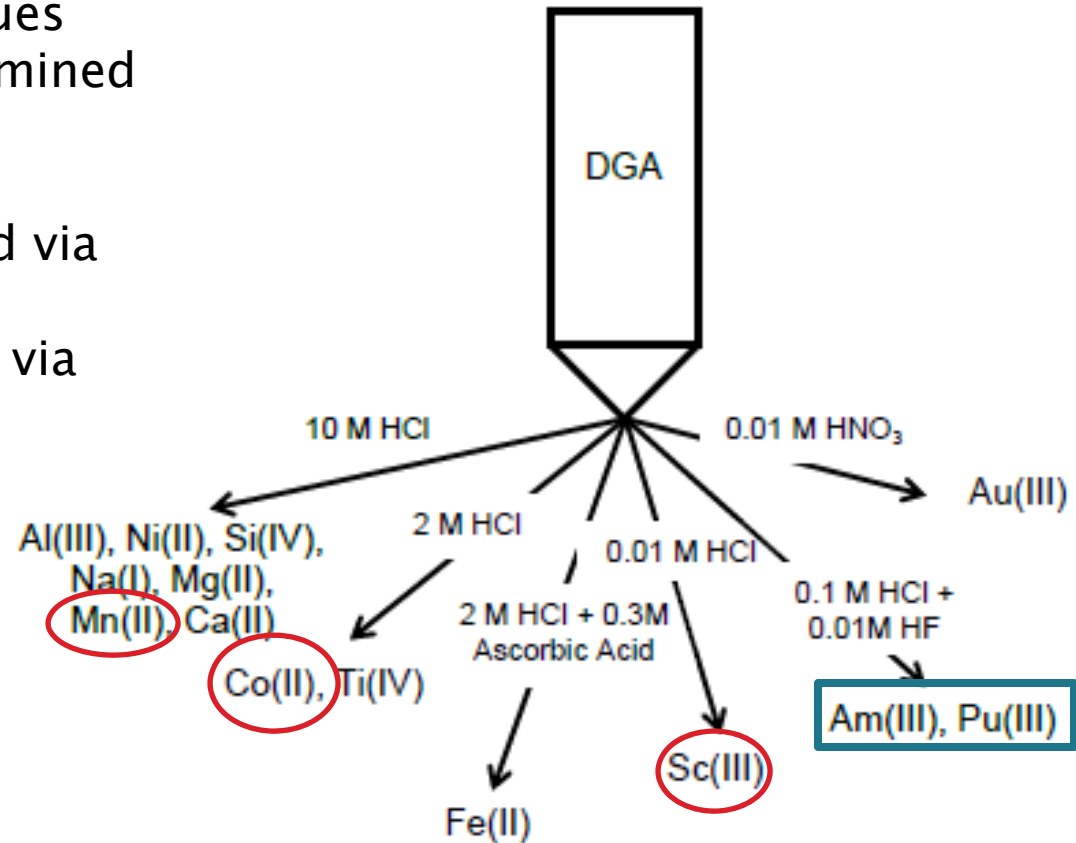
**¹⁹⁷Au, elastic scattering $\sigma=2.6354\text{b}$ and $n,2n \sigma=2.1323\text{b}$

¹⁹⁶Au, $\text{inl}=0.193\text{b}$ and $n,2n=1.975578\text{b}$

¹⁹⁵Au, $n-2n=0.8849\text{b}$ or $n,p=0.003083\text{b}$

Proposed Separation Scheme

- Based on literature k' values and experimentally determined k' values
- 10 mL DGA column
- Circled elements analyzed via gamma spectroscopy
- Stable elements analyzed via ICP-AES



Elution Profile for Detectable Activation Products

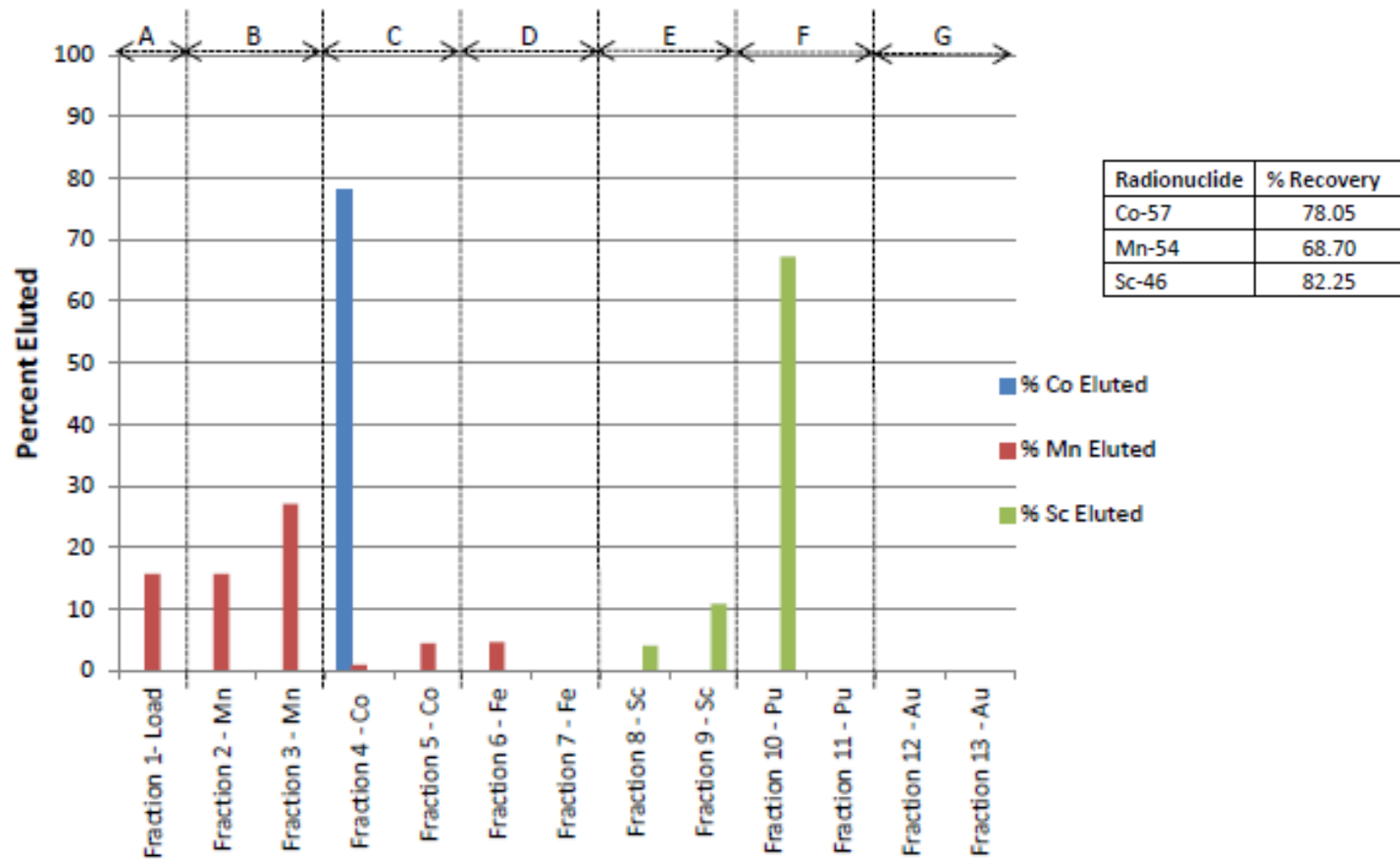


Figure 112. Glass/Cement Bead Separation Co, Mn, and Sc Elute Profiles
 All fractions are in 25 mL volumes. Mobile phases are as follows: A: 11 M HCl, B: 10 M HCl, C: 2 M HCl, D: 2 M HCl + 0.3 M Ascorbic Acid, E: 0.1 M HCl, F: 0.1 M HCl + 0.01 M HF, G: 0.01 M HNO₃

Elution Profile for all Components

| | Al (%) | Au (%) | Ca (%) | Fe (%) | Mg (%) | Na (%) | Ni (%) | Ti (%) | Mn-54 (%) | Co-60 (%) | Sc-46 (%) |
|---|--------|--------|--------|--------|--------|--------|--------|--------|-----------|-----------|-----------|
| Fraction 1: Load | 72.8 | 0 | 99.4 | 0 | 82.5 | 33.4 | 82.3 | 13.4 | 14 | 0 | 0 |
| Fraction 2: 11 M HCl | 0.0 | 0 | 0.6 | 0 | 0.0 | 20.5 | 0.0 | 0.0 | 16 | 0 | 0 |
| Fraction 3: 11 M HCl | 27.2 | 0 | 0.0 | 0 | 17.5 | 32.9 | 17.7 | 19.8 | 28 | 0 | 0 |
| Fraction 4: 2 M HCl | 0.0 | 0 | 0.0 | 0 | 0.0 | 13.2 | 0 | 66.8 | 1 | 78.1 | 0 |
| Fraction 5: 2 M HCl | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 4 | 0 | 0 |
| Fraction 6: 2 M HCl + 0.3 M Ascorbic Acid | 0.0 | 0 | 0.0 | 52.4 | 0.0 | 0.0 | 0 | 0 | 5 | 0 | 0 |
| Fraction 7: 2 M HCl + 0.3 M Ascorbic Acid | 0.0 | 0 | 0.0 | 6.5 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 |
| Fraction 8: 0.1 M HCl | 0.0 | 0 | 0.0 | 41.0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 4 |
| Fraction 9: 0.1 M HCl | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 11 |
| Fraction 10: 0.1 M HCl + 0.01 M HF | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 67 |
| Fraction 11: 0.1 M HCl + 0.01 M HF | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 |
| Fraction 12: 0.01 M HNO3 | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 |
| Fraction 13: 0.01 M HNO3 | 0.0 | 0 | 0.0 | 0 | 0.0 | 0.0 | 0 | 0 | 0 | 0 | 0 |

Foils are highlighted in green

Glass Components highlighted in purple

Activation Products highlighted in pink

Conclusions

- ▶ More work is needed refine larger constituents in the glass bead
 - Include more rinsing
- ▶ Investigate each activation products individual elution profile in the complex sample matrices
- ▶ Optimize column size and elution volumes



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Any Questions?

